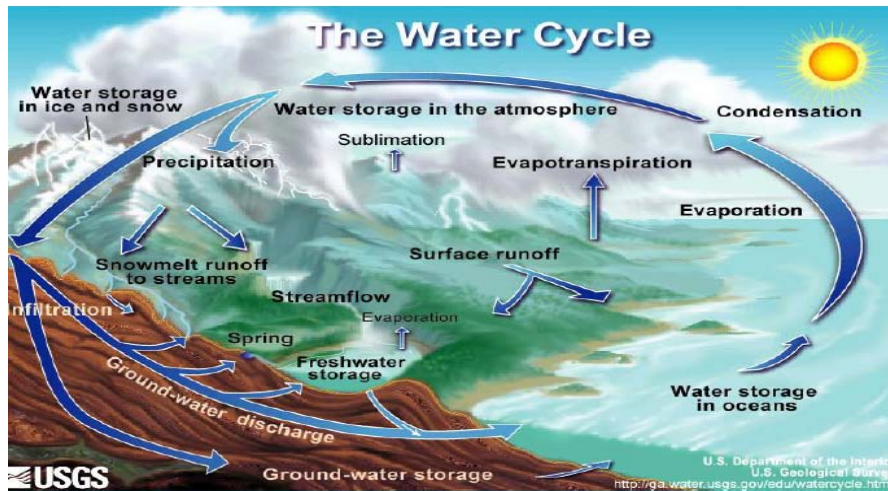


## Answers of Assignment 2: Engineering Hydrology

### 1- Application for engineering hydrology

- A) Flood forecasting
- B) Flood protection
- C) Flood routing
- D) Design of hydraulic structures
- E) Water resources and water management

### 2- Hydrologic Cycle



$$3- RH = \frac{e_v}{e_s} \%$$

$$= \frac{40}{e_s} \%$$

$$e_s = 611 e^{\frac{17.27 \times T}{237.3 + T}}$$

$$e_s = 611 e^{\frac{17.27 \times 30}{237.3 + 30}}$$

$$= 4251.8 \text{ Pascal}$$

$$= 42.52 \text{ mbar}$$

$$\text{Then } RH = 40/42.52 * 100 = 94.07 \%$$

$$4- e_s = 611 e^{\frac{17.27 \times T}{237.3 + T}}$$

$$e_s = 611 e^{\frac{17.27 \times 20}{237.3 + 20}}$$

$$= 2339.05 \text{ Pascal}$$

$$RH = \frac{e_v}{e_s} \% = 44\% \quad \longrightarrow \quad e_v = 1029.2 \text{ Pascal}$$

$$\text{At Dew point } e_v = e_s$$

$$1029.2 = 611 e^{\frac{17.27 \times T}{237.3 + T}}$$

$$\ln \frac{1029.2}{611} = \frac{17.27 \times T}{237.3 + T}$$

$$T = 7.39^\circ \text{C}$$

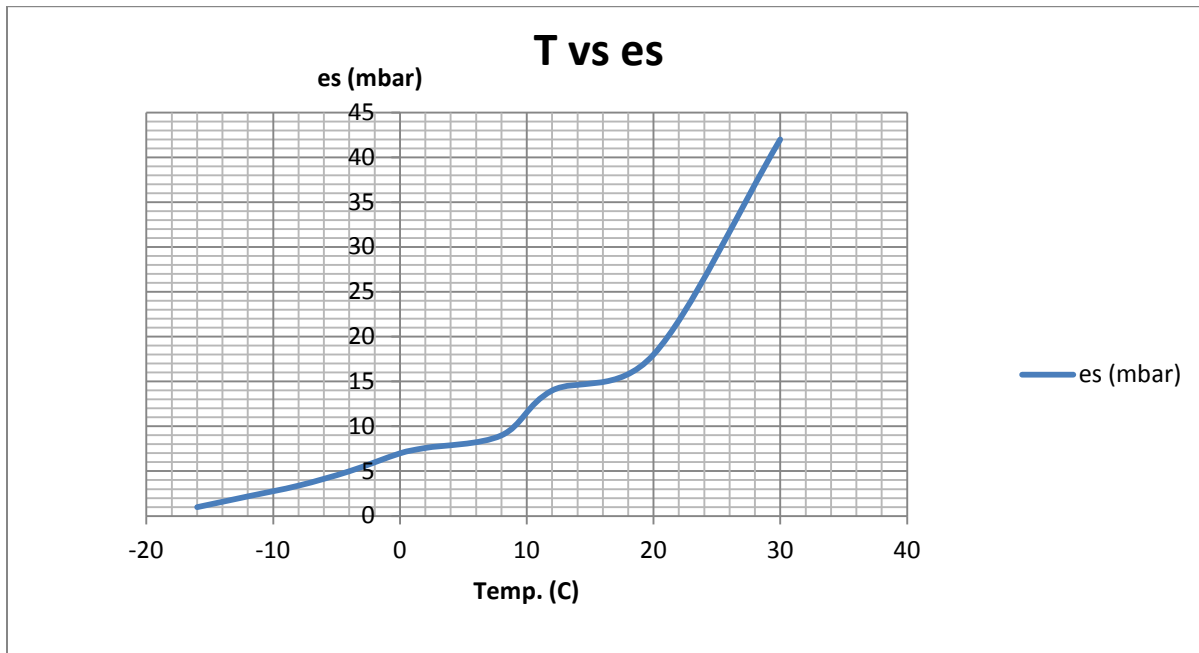
$$5 - \text{At } T = 6^\circ \text{C } e_v = e_s = 611 * e^{\frac{17.27 T}{237.3 + T}} = 611 * e^{\frac{17.27 * 6}{237.3 + 6}} = 935.41 \text{ Pascal}$$

$$\text{At } T = 20^\circ \text{C} \quad e_s = 611 * e^{\frac{17.27 T}{237.3 + T}} = 611 * e^{\frac{17.27 * 20}{237.3 + 20}} = 2339 \text{ Pascal}$$

$$\therefore RH = \frac{e_v}{e_s} \times 100 = \frac{935.41}{2339} \times 100 = 40 \%$$

6 -

a)



b) At T 16°C  $e_s = 15$  mbar (from the curve or by using the previous equation)

$$RH = 40 \% = \frac{e_v}{e_s} \times 100 = \frac{e_v}{15} \times 100 \quad \therefore e_v = 6 \text{ mbar} = 600 \text{ Pascal}$$

$$\text{At dew point } e_v = e_s = 611 * e^{\frac{17.27 T}{237.3 + T}} = 600$$

$$\therefore T = -0.23 \text{ } ^\circ\text{C}$$

c)  $e_v = 16$  mbar

$$\text{At dew point } e_v = e_s = 611 * e^{\frac{17.27 T}{237.3 + T}} = 1600 \text{ Pascal}$$

$$\therefore T = 17 \text{ } ^\circ\text{C}$$

**7 –**

$$T = 23^\circ\text{C}, e_v = 10 \text{ mbar}, K = 0.3, W_{18} = 18 \text{ m/s}$$

$$e_s = 611 * e^{\frac{17.27 T}{237.3 + T}} = 611 * e^{\frac{17.27 * 23}{237.3 + 23}} = 2810.35 \text{ Pascal} = 21.17 \text{ mmHg (1mmHg=133Pa)}$$

$$e_v = 10 \text{ mbar} = 1000 \text{ Pascal} = 7.51 \text{ mmHg}$$

$$RH = \frac{e_v}{e_s} \times 100 = \frac{7.51}{21.17} \times 100 = 35.5 \%$$

$$\left(\frac{W_8}{W_{18}}\right) = \left(\frac{Z_8}{Z_{18}}\right)^K \quad \therefore \left(\frac{W_8}{18}\right) = \left(\frac{8}{18}\right)^{0.3} \quad \therefore W_8 = 14.11 \text{ m/s} = 50.8 \text{ km/hr}$$

$$\therefore E = 0.5 * 21.17 * \left(1 - \left(\frac{35.5}{100}\right)\right) * (1 + 0.0625 * 50.8) = 28.33 \text{ mm/day}$$

**8 –**

$$E.T = K_s * K_c * E = 0.7 * 0.85 * 28.33 = 16.85 \text{ mm/day}$$

**9- Given:**  $W_o = 40 \text{ km/h}$        $Z_o = 100 \text{ m}, Z = 10 \text{ m}$        $K = 0.2$

**Required:**

$$W = ? \text{ mph}$$

**Solution:**

$$W_1/W_o = (Z_1/Z_o)^K$$

$$W_1/40 = (10/100)^{0.2}$$

$$W = 25.238 \text{ km/h} = 40.63 \text{ mph} \quad (1 \text{ mph} = 1.61 \text{ km/h})$$

**10- Given:**  $Z_o = 5 \text{ m}$        $W_o = 5 \text{ m/s}, Z_1 = 60 \text{ m}$        $W_1 = 10 \text{ m/s}$

**Required:**

$$\text{Wind speed at } Z=10 \text{ m \& } Z=30 \text{ m}$$

**Solution:**

$$W_1/W_o = (Z_1/Z_o)^K$$

$$10/5 = (60/5)^K$$

$$K = 0.279$$

For  $Z_2 = 10$  m

$$W_2/W_o = (Z_2/Z_o)^K$$

$$W_2/5 = (10/5)^{0.279}$$

$$W_2 = 6.067 \text{ m/sec}$$

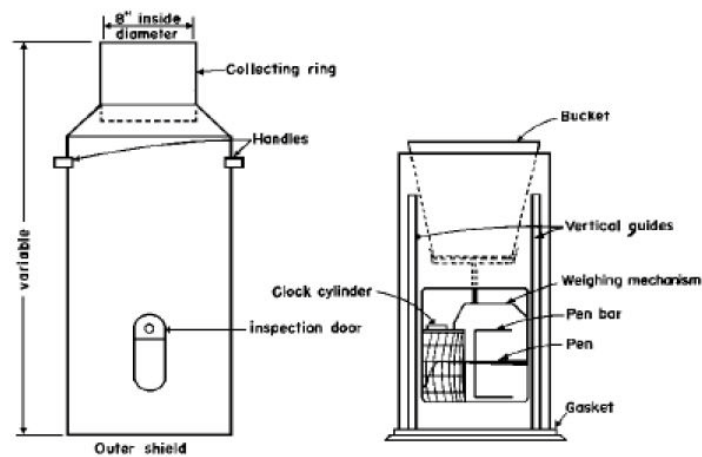
For  $Z_3 = 30$  m

$$W_3/W_o = (Z_3/Z_o)^K$$

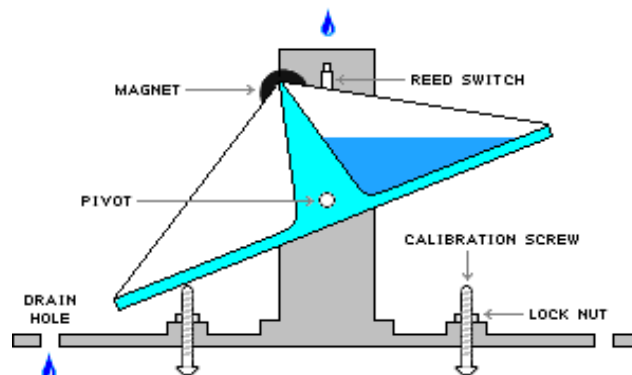
$$W_3/5 = (30/5)^{0.279}$$

$$W_3 = 8.24 \text{ m/sec}$$

**11-**



### 1) Weighing Bucket Type



### 2) Tipping Bucket Type

## 12- Factors affecting infiltration:

1) Soil characteristics:

Soil type, porosity, moisture content and land use.

2) Land cover.

3) The characteristics of infiltrated water:

Such as low temperature which lowers water viscosity that means higher infiltration rate.

4) Land slope.

5) The amount of precipitated water.

13-

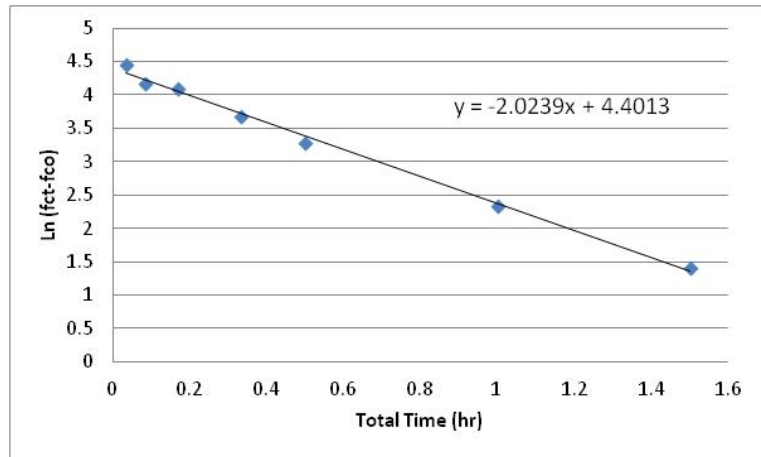
T (min)	T in hr	V <sub>total</sub> (cm <sup>3</sup> )	ΔV increment(cm <sup>3</sup> )	Δd increment(cm)	Δd increment(m)
0	0	0	0	0	0
2	0.033333	300	300	0.311813782	3.118137823
5	0.083333	650	350	0.363782746	3.63782746
10	0.166667	1190	540	0.561264808	5.612648082
20	0.333333	1950	760	0.789928249	7.899282485
30	0.5	2500	550	0.571658601	5.716586009
60	1	3350	850	0.883472383	8.834723832
90	1.5	3900	550	0.571658601	5.716586009
150	2.5	4600	700	0.727565492	7.275654921

ΔT: Time increment (min.)	ΔT: Time increment (hr)	F <sub>ct</sub> (mm/hr) = Δd/ΔT
0	0	0
2	0.033333	93.544135=F <sub>co</sub>
3	0.05	72.756549
5	0.083333	67.351777
10	0.166667	47.395695
10	0.166667	34.299516
30	0.5	17.669448
30	0.5	11.433172
60	1	7.2756549=F <sub>cf</sub>

X (T in hr)	Y (ln(f <sub>ct</sub> -f <sub>cf</sub> ))
0	0
0.033333	4.457460291
0.083333	4.18175314
0.166667	4.095606715
0.333333	3.691867359
0.5	3.296707452
1	2.341175575
1.5	1.42483504

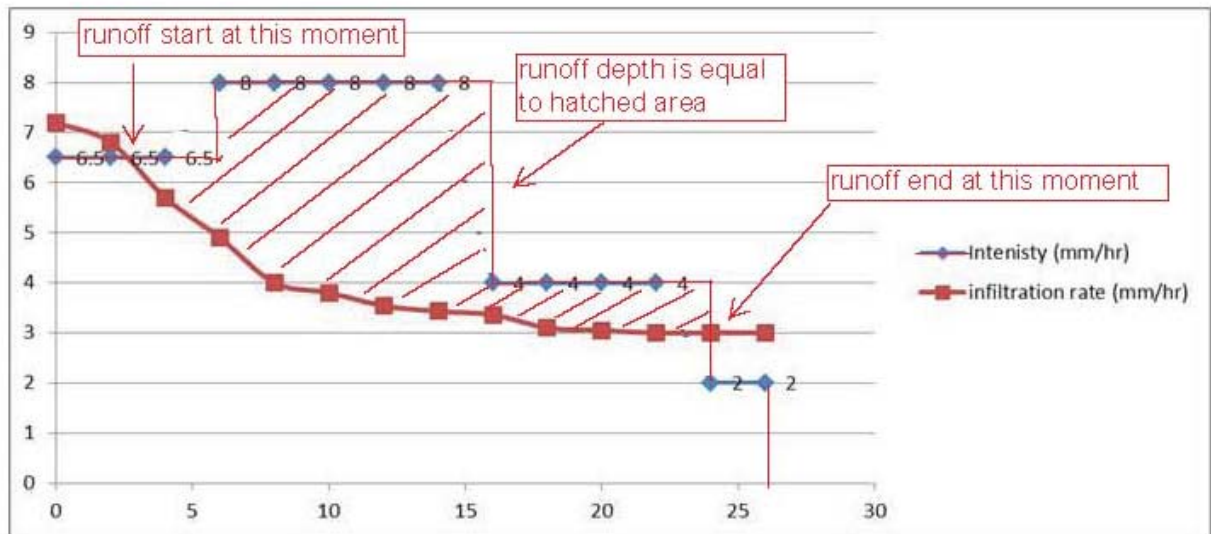
$F_{co} = 93.544 \text{ mm/hr}$   
 $F_{cf} = 7.276 \text{ mm/hr}$   
 Horton's Equation:  
 $F_{ct} = F_{cf} + (F_{co} - F_{cf})e^{-kt}$   
 $\ln(F_{ct} - F_{cf}) = \ln(F_{co} - F_{cf}) - kt$   
 $Y = C - mx$   
 Then  $K = 2.02 \text{ hr}^{-1}$

Or by substituting with  
 different T &  $F_{ct}$  to get  
 different K values and  
 taking the avg.



14-

time(hr)	Intenisty (mm/hr)	infiltration rate (mm/hr)
0.01	6.5	7.2
2	6.5	6.8
4	6.5	5.7
6	8	4.9
8	8	4
10	8	3.8
12	8	3.54
14	8	3.43
16	4	3.36
18	4	3.1
20	4	3.05
22	4	3
24	2	3
26	2	3



Run off depth = sum (intensity – average infiltration rate )\* 2hr  
= 52.44mm or area over the curve.

**15-**

$$V_{in} - v_{out} = \Delta \text{ Storage}$$

$$V_{in} = \text{inflow} + \text{precipitation}$$

$$V_{in} = 200,000 \text{ m}^3/\text{day} * 30 \text{ days} \\ + (10.5\text{cm}/100) * (500 \text{ hectare} * (10^4))$$

$$V_{in} = 6,525,000 \text{ m}^3$$

$$V_{out} = \text{seepage} + \text{evaporation}$$

$$V_{out} = (2\text{cm}/100) * (500 \text{ hectare} * (10^4)) \\ + (8.5\text{cm}/100) * (500 \text{ hectare} * 10^4) + 30Q_{out}$$

$$V_{out} = 525,000 + 30Q_{out} \text{ m}^3$$

$$\Delta \text{ Storage} = -(0.5 * 500 \text{ hectare} * 10,000)$$

$$= -2,500,000 \text{ m}^3$$

$$6,525,000 - 525,000 - 30Q_{out} = -2,500,000$$

$$Q_{out} = 283,333.3 \text{ m}^3/\text{d}$$

**16-**

$$\Delta \text{Vol.}_{\text{Storage}} = V_{\text{in}} - V_{\text{out}}$$

$$\text{Runoff Coeff.} = R/P = 0.45$$

$$V_{\text{in}} = \text{Runoff into the reservoir}$$

$$= (0.45 * (50 \text{ mm} / 1000) * ((1.9 * 10^6) \text{ km}^2 * 10^6 \text{ m}^2))$$

$$= 4.275 * 10^{10} \text{ m}^3$$

$$\Delta \text{Vol.}_{\text{Storage}} = (2 * 10^{-6}) * (178^{7.46} - 175^{7.46}) = 1.46 * 10^{10} \text{ m}^3$$

$$\Delta \text{Vol.}_{\text{Storage}} = V_{\text{in}} - V_{\text{out}}, \quad V_{\text{out}} = V_{\text{evaporation}}$$

$$1.46 * 10^{10} \text{ m}^3 = 4.275 * 10^{10} \text{ m}^3 - V_{\text{evap.}}$$

$$\text{Then } V_{\text{evap.}} = 2.815 * 10^{10} \text{ m}^3$$

$$\text{Then } V_{\text{evap.}} = 2.815 * 10^{10} \text{ m}^3 / (5500 * 10^6 * 30) * 1000 = 170.6 \text{ mm/d}$$